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⑷ Hydraulic braking system.

⑸ An hydraulic braking system includes a primary pressure source (1) connected to a brake actuator and operable by a force input device (2). A fluid displacer (8) is actuated by an electrical stepper motor (11) operated by a controller (13) in response to action of said device 2, as sensed by a sensor (14). Fluid displaced from the displacer (8) is added to that displaced from the primary pressure source for application to the actuator. By suitable programming of the controller, servo-assistance and/or quick-fill modes can be produced by the displacer (8) and a wheel-slip correction facility can also be provided.

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HYDRAULIC BRAKING SYSTEM.

This invention relates to an hydraulic braking system, primarily for a motor vehicle.

In one prior proposal, electric motors used to generate a primary braking force applied directly to braking elements are actuated by a control system in response to operation of a brake pedal which also actuates a back-up master cylinder, the latter becoming fully effective only in the event of an electrical system failure. In such a system, jamming of an electric motor or any associated force transmission mechanism in the brakes-applied condition could result in the associated brake being locked on. Not only is such a situation potentially dangerous, but some dismantling of the brake would be required to free the jammed component giving rise to considerable inconvenience.

An object of the invention is to provide a braking system in which this problem is avoided and which provides additional advantages in terms of flexibility of control and the possibility of using compact components.

According to the invention, a braking system comprises a primary hydraulic pressure source connected to a brake actuator and operable by a force input device, and a fluid displacer actuated by an electrical stepper motor operated by controller in response to action of said force input device, the arrangement being such that fluid displaced from the fluid displacer is added to that displaced from the primary pressure source for application to the brake actuator.

In such a system, the pressure generated at the actuator is always dependent upon the primary actuating pressure, enabling good braking balance to be obtained. Moreover, in the event of electrical or mechanical failure occurring in the stepper motor or fluid displacer, adequate braking pressure is still available from the primary pressure source.

The additional fluid volume from the fluid displacer is useful primarily to provide a servo-assistance effect at the brake actuator and/or a quick-fill facility. The precise functioning of the displacer in one or both of, or as between these roles, is dependent upon the motor speed controlled by suitable programming of the controller.

It may be convenient to interpose one or more electrically operated cut-off valves between the primary pressure source and the actuator, enabling the primary pressure source to be isolated from the actuator upon actuation of the valve. It is then possible to control the motor in response to the detection of an incipient wheel slip condition occurring on wheel associated with the brake actuator, (which condition may result from spinning or skid-

ding of the wheel) enabling the fluid displacer to be actuated in a manner such as to de-boost or pressurise the actuator in order to correct the slip condition, and subsequently to restore normal braking pressure.

In one convenient arrangement, the primary pressure source is a pressure cylinder actuated by force input means, such as a brake pedal, and the fluid displacer is a piston axially reciprocable under the action of the stepper motor to vary the volume of a fluid chamber.

The invention will now be described, by way of example, with reference to the accompanying drawing which is a diagrammatic representation of one form of the hydraulic braking system of the invention.

Referring to the drawing, the braking system shown therein includes a primary hydraulic pressure source in the form of a master cylinder 1 actuated by a lever 2 which may conveniently be a driver-operated brake pedal pivoted at 3 on fixed structure 4, being normally part of a vehicle body. The master cylinder is connected by a line 5 to an electrically operated solenoid valve 6 which is normally open to permit pressurised fluid from the master cylinder to enter a supply line 7 to a brake actuator 7A. The supply line 7, in the arrangement illustrated, is incorporated in a fluid displacer device 8 to which the valve 6 is connected and which includes an axially reciprocable piston 9 partly defining a chamber 10. The piston is driveable by a stepper motor 11 via a conventional form of efficient screw coupling mechanism, part of which can be seen at 12, such that rotation of the motor causes corresponding linear movement of the piston. The motor operates under the influence of an electronic controller 13 to which signals are fed from a displacement sensor 14 actuated by the pedal 2. The controller also receives signals from a wheel speed and/or acceleration sensor associated with the wheel to be braked and activates the solenoid valve 6 via an electrical connection 6A upon the detection of an incipient wheel slip condition by the sensor.

For normal braking operations, the solenoid valve 6 is de-energised, placing the master cylinder 1 in direct communication via the passages 5 and 7 with the brake actuator. Actuation of the pedal lever 2 operates the master cylinder 1 in conventional manner and supplies braking fluid under pressure to the brake. Simultaneously, the pedal lever displacement is sensed by the sensor 14 and a corresponding electrical signal is supplied to the controller which, in turn, operates the motor 11 in a direction such as to move the piston 9 in-

wardly to pressurise the fluid in the chamber 10. The resulting displaced fluid volume is added to that supplied by the master cylinder and effectively provides servo-assistance to the braking action. Since the operation of the piston is dependent upon pedal travel, the servo effect increases with increased pedal displacement, and vice versa.

It is possible for the motor 11 and piston 9 to perform functions other than or additional to the servo-assistance role described. For example, by programming the controller to move the piston at a higher rate over at least an initial portion of its travel, a relatively large volume of fluid may rapidly be injected into the actuator, enabling it to effect a rapid take-up of braking clearances, prior to the application of large braking forces. Once the taking up of clearances has been completed, the piston may be controlled to provide the servo-assistance mode described above, or any other useful function.

By arranging for the piston 9 to provide the larger part of the required braking effort, it is possible to use a master cylinder of very compact proportions, as compared with conventional master cylinders. It will be possible, for example, to supply three parts of the required volume by means of the motor-driven piston and one part from the master cylinder.

The system described can also operate in an anti-skid mode. Upon the sensing by the wheel sensor of an incipient wheel skid condition at the braked wheel, the controller produces a signal to energise the solenoid valve 6 in order to isolate the master cylinder 1 from the brake actuator. Simultaneously, or shortly thereafter, the motor is energised to move the piston 9 to the left, as seen in the drawing, in order to enlarge the volume of the chamber 10 and thereby de-boost the brake actuator in order to release the brake. Once the skid condition is corrected, the motor is operated in the reverse direction to re-pressurise the actuator and the solenoid valve 6 is de-energised to reconnect the master cylinder to the brake. Normal braking then ensues, accompanied by the servo-effect produced by the piston 9.

The solenoid valve 6 is normally held in its open position, conveniently by the action of a spring which is overcome when the solenoid is energised to close the valve. This provides a convenient fail safe arrangement, enabling the master cylinder to be placed immediately in communication with the brake in the event of power failure, in order to maintain normal braking. Because of the non-operation of the piston 9, the master cylinder 1 would be required to produce additional fluid volume and the input member 2 would therefore be subject to greater displacement than normal.

It is important that the position of the armature

of the motor 11, and therefore the piston 9, should have a known datum position which can be used by the controller and means are provided in the system to enable the controller to establish the datum, for example by moving the piston 9 against an abutment during periods when the system is non-operative, in order to check and re-establish the datum position.

The system described can readily be adapted to provide traction control by correcting excessive wheel spin which can occur under certain conditions. For this purpose, the controller 13 is programmed to respond to signals indicative of excessive wheel spin and operates the motor in a direction such as to move the piston 9 to the right, as seen in the drawing, in order to increase the pressure in the brake actuator connected to the chamber 10. The controller also closes the valve 6 in order to isolate the master cylinder 1 from the brake during the traction control mode. Alternatively, if the design of the valve 6 makes such isolation impossible or unreliable when the valve is under pressure from the displacer 8, it is possible to provide an additional solenoid valve means disposed between and in series with the master cylinder 1 and valve 6 and connected to the controller so as to be closed by a signal from the latter when traction control is required in order to prevent pressure developed in the chamber 10 for traction control from being applied to the master cylinder. In an alternative arrangement, the additional valve may be in a common housing with the valve 6. The valve 6, or that part operative in the anti-skid mode will normally be open during traction control operation.

Again, by suitable programming of the controller, the system of the invention may be operated to provide a "hill hold" facility. This would normally operate with a vehicle stationary on an incline and with the vehicle in gear and clutch disengaged. An appropriate signal sent from the controller to the motor under these conditions causes the piston 9 to be advanced to pressurise one or more brake actuators so as to prevent the vehicle from running backwards down the hill. Brake pressurisation would again be accompanied by isolation of the master cylinder in the manner required for traction control described above. The brake(s) would be released as the clutch is engaged.

Although the invention has been described in relation to a single brake actuator, it will be understood that a typical practical braking system would have at least two master cylinder chambers feeding any convenient number of brake lines and any desired number of wheel slip correction channels could be established to control the brake lines in a desired manner.

Claims

1. A braking system comprising a primary hydraulic pressure source (1) connected to a brake actuator (7A) and operable by a force input device (2), and an electric motor (11) operable by electric control means (13) in response to operation of the force input device to generate braking force at said brake actuator, characterised in that said electric motor is a stepper motor (11) which actuates a fluid displacer (8) under the influence of control means (13) in response to action of said force input device (2), such that fluid displaced from the fluid displacer (8) is added to that displaced from the primary pressure source (1) for application to the brake actuator (7A). 10
2. A braking system according to Claim 1, characterised in that the fluid displacer (8) is actuated by said motor (11) in a quick-fill and/or servo-assistance mode by appropriate speed control of the motor from said control means (13). 15
3. A braking system according to Claim 1 or Claim 2, characterised in that a cut-off valve (6) is interposed between the primary pressure source (10) and the brake actuator (7A) and is operable to isolate the source (1) from the actuator in response to a slip condition of a wheel to be braked, said fluid displacer being actuated to vary the braking pressure in the actuator in order to correct the slip condition. 20
4. A braking system according to Claim 3, characterised in that the cut-off valve (6) is an electrically operated solenoid valve actuated by said control means. 25
5. A braking system according to any one of the preceding claims, characterised in that the fluid displacer includes a piston (9) reciprocable by said motor (11) to vary the volume of a pressure chamber (10) of the displacer connected to the brake actuator (7A) in order to modify the braking pressure in the actuator. 30
6. A braking system according to Claim 5, characterised in that the piston (9) is connected to the motor (11) by a screw coupling mechanism (12) whereby rotation of the motor causes corresponding linear movement of the piston. 35
7. A braking system according to Claim 6, characterised in that the piston (9) is hollow and internally threaded to receive a correspondingly threaded shaft (12) in driving engagement, said shaft being drivable in rotation by the motor (11). 40
8. A braking system according to any one of the preceding claims, characterised in that a travel sensor (14) is actuated by the force input device (2) and supplies a signal to the control means (13) representative of pedal travel. 45

9. A braking system according to any one of Claims 5 to 8, characterised in that fluid output from the primary pressure (1) source is directed to said pressure chamber (10) from which it flows via an outlet (7) of the chamber to the brake actuator. 50



